

Motion Constraints

Even if $\bar{q}$ is minimal, the generalized speeds $u_1, \dots, u_n$ may not be independent. (This property of the system not the choice of the u 's). If the u 's are not independent the system S is subject to motion constraints (non-holonomic constraints).

There is a special kind of non-holonomic systems called a simple non-holonomic system where:

$$u_r = \sum_{s=1}^p A_{rs} u_s + B_r \quad r = p+1, \dots, n$$

$\nwarrow$ dependent G.S. $\nearrow$ independent G.S.
 $\nwarrow$ linear dependence

$\underbrace{\hspace{10em}}_{m \text{ items}}$

$$p = n - m$$

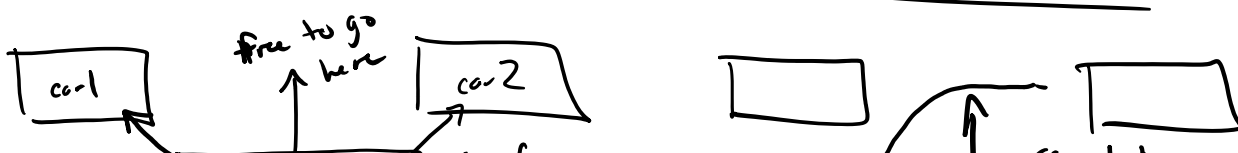
$\uparrow$ # ind. G.S.s $\uparrow$ # min. G.S.s $\uparrow$ m dep G.S.s
 $\uparrow$ total # of G.S.

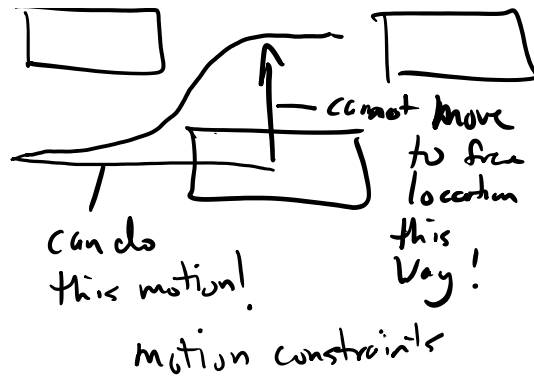
$$\bar{u} = \begin{bmatrix} u_1 \\ \vdots \\ u_p \\ u_{p+1} \\ \vdots \\ u_n \end{bmatrix} \left\{ \begin{array}{l} p \\ m \end{array} \right\} \left\{ n \right.$$

- Configuration constraints
 - reduces # of independent G.G's
 - Holomic constraints
 - constrain where the system can go

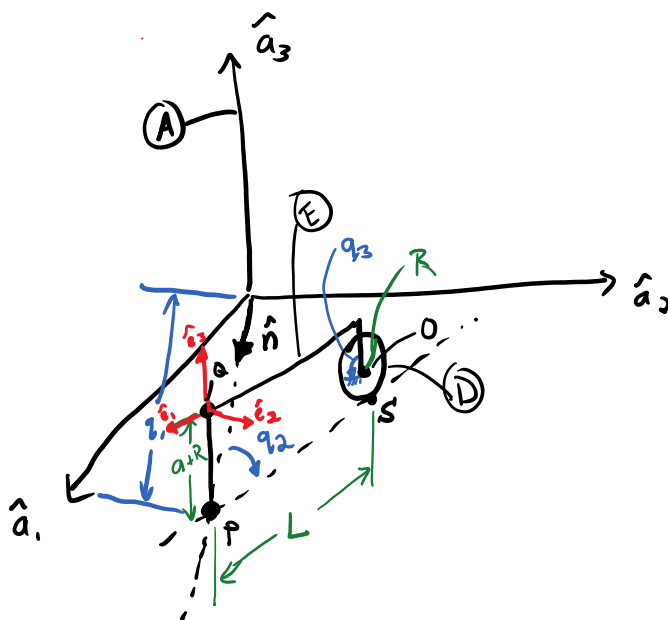
essential

- Motion constraints
 - reduces # DoF and # independent G.S's
 - Non-holomic constraints
 - constrain how the system can go where you want it to





Simple trailer roll w/o slip on a ground plane


$$n=3$$

$$\hat{e}_3 = \tilde{q}_3$$

$$\hat{n} = c_2 \hat{e}_1 + s_2 \hat{e}_2$$

$${}^A\overline{V}^P = \dot{q}_1 \hat{n} \quad {}^A\overline{V}^Q = \dot{q}_1 \hat{n}$$

$$A - \frac{0}{V} = A - \frac{Q}{V} + A - \frac{E}{\omega} \times \frac{r}{r} \% Q$$

$$= \dot{q}_1 \hat{n} - \dot{q}_3 \hat{e}_3 \times (-L \hat{e}_1 - a \hat{e}_3)$$

$${}^A \bar{V}^0 = \dot{q}_1 c_2 \hat{e}_1 + (\dot{q}_1 s_2 + L \dot{q}_3) \hat{e}_2$$

$A \bar{V}^S = 0$ if there is pure rolling
 S is fixed in D

$$A \bar{V}^S = A \bar{V}^O + A \bar{\omega}^D \times \bar{r}^{S/O}$$

$$A \bar{V}^S = A \bar{V}^O + (\dot{q}_3 \hat{e}_2 - \dot{q}_2 \hat{e}_3) \times (-R \hat{e}_3)$$

$$A \bar{V}^S = (\dot{q}_1 c_2 - R \dot{q}_3) \hat{e}_1 + (\dot{q}_1 s_2 + L \dot{q}_2) \hat{e}_2 = 0$$

$$\left. \begin{aligned} A \bar{V}^S \cdot \hat{e}_1 = 0 &= \dot{q}_1 c_2 - R \dot{q}_3 \quad (1) \\ A \bar{V}^S \cdot \hat{e}_2 = 0 &= \dot{q}_1 s_2 + L \dot{q}_2 \quad (2) \end{aligned} \right\} 2 \text{ motion constraints}$$

Are these essential motion constraints?

$$\frac{df}{dt} = \frac{\partial f}{\partial q_1} \dot{q}_1 + \frac{\partial f}{\partial q_2} \dot{q}_2 + \frac{\partial f}{\partial q_3} \dot{q}_3 + \frac{\partial f}{\partial t} = 0$$

$$(1) \quad \frac{\partial f}{\partial q_1} = \cos q_2 \quad \frac{\partial f}{\partial q_2} = 0 \quad \frac{\partial f}{\partial q_3} = -R$$

$$\frac{\partial f}{\partial q_2 \partial q_1} = -\sin q_2 \quad \frac{\partial f}{\partial q_1 \partial q_2} = 0 \quad \times \quad \text{doesn't commute essential!!}$$

$$\frac{\partial f}{\partial q_1 \partial q_3} = 0 \quad \frac{\partial f}{\partial q_3 \partial q_1} = 0 \quad \checkmark$$

$$\frac{\partial f}{\partial q_1 \partial q_2} = 0 \quad \frac{\partial f}{\partial q_2 \partial q_1} = 0 \quad \checkmark$$

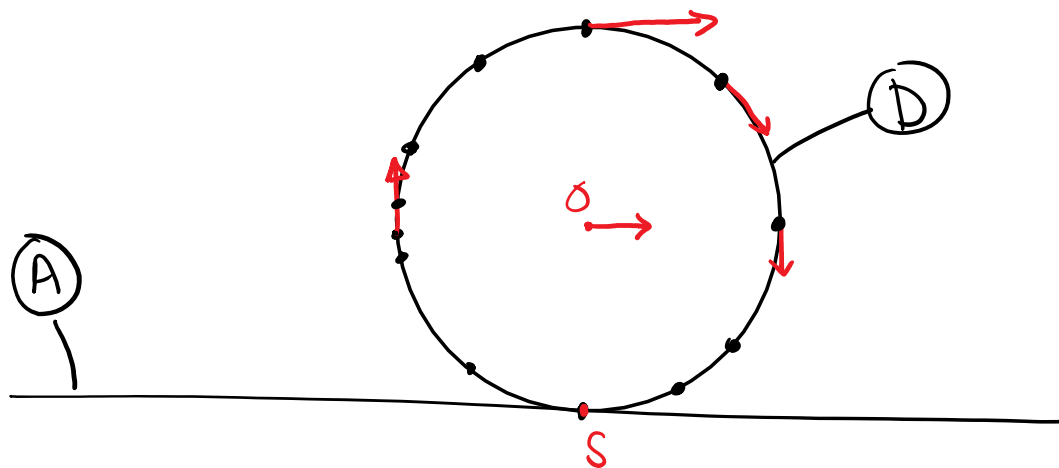
$$(2) \quad \frac{\partial f}{\partial q_1} = \sin q_2 \quad \frac{\partial f}{\partial q_2} = L$$

$$\frac{\partial f}{\partial q_1 \partial q_2} = 0$$

$$\frac{\partial f}{\partial q_2 \partial q_1} = \cos q_2 \quad \times$$

essential!

$$g(u_1, \dots, u_n, q_1, \dots, q_n, t) = 0 \quad \text{potential motion constraint}$$



Summary of GC's, GS's, and constraints

- $n + n^*$ generalized coordinates used to describe a system S 's configuration
- there may be dependent generalized coordinates that arise from holonomic configuration constraints $\bar{f}(\underbrace{q_1, \dots, q_n}_{\text{ind.}}, \underbrace{q_{n+1}, \dots, q_{n+n^*}}_{\text{dep}}, t) = 0$, such that there are n independent GC's and n^* dependent GC's.

$$\bar{f} \in \mathbb{R}^{n^*} \quad \bar{f}: n^* \times 1$$

- given the minimal # of GC's $\bar{q} = [q_1, \dots, q_n]^T$ you can define generalized speeds $\bar{u} = [u_1, \dots, u_n]^T$ such that

$$\pi \quad \forall \dot{\bar{q}} + \bar{z} \quad \text{or} \quad u_r = \sum_{s=1}^n \gamma_{rs} \dot{q}_s + z_r \quad r=1, \dots, n$$

then

$$\bar{u} = Y \dot{q} + \bar{z}$$

matrix form

$$u_r = \sum_{s=1}^n Y_{rs} \dot{q}_s + z_r \quad r=1, \dots, n$$

scalar form

Y must be invertible (Y^{-1}) for your choice of GS's to be legitimate, i.e. $\dot{q} = Y^{-1}(\bar{u} - \bar{z})$ for all time
 kinematical diff. eqn.

- If no motion constraints, then $n=p$, i.e. # min. GC's = # Dof resulting in n independent u 's, n independent q 's, and thus $2n$ first order differential equations in time.

$$n \times 1 \quad \dot{\bar{u}} = ? \quad \Rightarrow \text{come from } \bar{F} = m \bar{a}$$

$$n \times 1 \quad \dot{\bar{q}} = Y^{-1}(\bar{u} - \bar{z})$$

not integrable

- If there are m essential motion constraints, the $p = n - m$ u 's are independent and m u 's are dependent. There will then be only p 1st order ODE's for the u 's:

$$p \times 1 \quad \dot{\bar{u}}_s = [\dot{u}_1, \dots, \dot{u}_p] = ?$$

$$n \times 1 \quad \dot{\bar{q}} = Y^{-1}(\bar{u} - \bar{z})$$

The dependent speeds are found from:

$$\bar{u}_r = A_{rs} \bar{u}_s + \bar{B}_r \quad \text{or} \quad u_r = \sum_{s=1}^p A_{rs} u_s + B_r \quad r=p+1, \dots, n$$

matrix

scalar form

Partial Velocities and Partial Angular Velocities

$q_1, \dots, q_n$ GC's

$u_1, \dots, u_n$ GS's

In general we have lots of rigid bodies, points, and particles whose motion we are interested in.

All velocities and angular velocities in the system can be expressed uniquely as linear functions of the u_i 's.

$$\bar{\omega} = \sum_{r=1}^{(n)} \bar{\omega}_r u_r + \bar{\omega}_t$$

$\nwarrow$ linear in the u 's
 $\nwarrow$ r th partial angular velocity
 $\nearrow$ remainder

$$\bar{v} = \sum_{r=1}^{(n)} \bar{v}_r u_r + \bar{v}_t$$

$\nwarrow$ linear in the u 's
 $\nwarrow$ r th partial velocity
 $\nearrow$ remainder

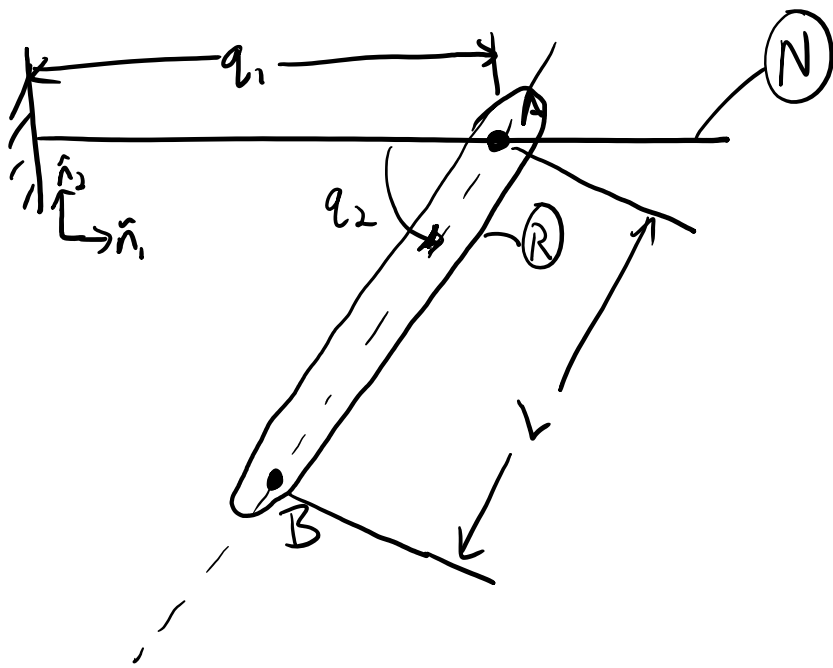
$\bar{\omega}_r, \bar{v}_r, \bar{\omega}_t,$ and $\bar{v}_t$ are all functions of $q_1, \dots, q_n, t$.

Note that $\bar{\omega}_r = \frac{\partial \bar{\omega}}{\partial u_r}$ and $\bar{v}_r = \frac{\partial \bar{v}}{\partial u_r}$

$\bar{\omega}_r$ and $\bar{v}_r$ are the sensitivities of $\bar{\omega}$ and $\bar{v}$ to u_r .

Example

1. $\xrightarrow{a} \rightarrow$ (N) $\sim$ GC's



$$\begin{aligned}
 n &= 2 & 2 \text{ GC's} \\
 m &= 0 \\
 p &= 2 & 2 \text{ DoF}
 \end{aligned}$$

$${}^N \bar{V}^A = \dot{q}_1 \hat{n}_1$$

$${}^N \bar{V}^B = \dot{q}_1 \hat{n}_1 + \dot{q}_2 \hat{n}_3 \times (-L c_2 \hat{n}_1 - L s_2 \hat{n}_2)$$

$${}^N \bar{V}^B = (\dot{q}_1 + L \dot{q}_2 s_2) \hat{n}_1 - L \dot{q}_2 c_2 \hat{n}_2$$

$${}^N \bar{\omega}^R = \dot{q}_2 \hat{n}_3$$

Choose some GS's.

$$u_1 = \dot{q}_1, \quad u_2 = \dot{q}_2$$

$${}^N \bar{\omega}^R = u_2 \hat{n}_3 \quad {}^B \bar{V}^A = u_1 \hat{n}_1$$

$${}^N \bar{V}^B = (u_1 + L u_2 s_2) \hat{n}_1 - L u_2 c_2 \hat{n}_2 = u_1 \hat{n}_1 + u_2 (L s_2 \hat{n}_1 - L c_2 \hat{n}_2)$$

Calculate the partial velocities

	u_1	u_2
${}^N \bar{\omega}^R$	0	$\hat{n}_3$
${}^N \bar{V}^A$	$\hat{n}_1$	0

$$\begin{array}{c|c|c} \tilde{N} \bar{V}^A & \hat{n}_1 & 0 \\ \hline N \bar{V}^B & \hat{n}_1 & L s_2 \hat{n}_1 - L c_2 \hat{n}_2 \end{array}$$

$$N \bar{V}_2^B \triangleq 2^{\text{nd}} \text{ partial velocity of } B \text{ in } N$$